

Description

The SARS01/05 is an auxiliary switch diode especially designed for snubber circuits, which are used in the primary sides of flyback switched-mode power supplies.

Being capable of reducing the ringing voltage generated at power MOSFET turn-off, the SARS01/05-incorporated snubber circuits allow better cross regulation of multiple outputs.

The SARS01/05 can also improve power supply efficiency by partially transferring such ringing voltage into the secondary side of a power supply unit.

Features

- Improves Cross Regulation
- Reduces Noise
- Improves Efficiency

Applications

For switched-mode power supplies (SMPS) with flyback topology such as:

- White Goods
- Adaptor
- Industrial Equipment

Typical Application



Package

• SARS01 Axial (φ2.7 × 5.0L / φ0.6)







Not to scale

Selection Guide

| Part Number | I _{F(AV)} | V _F (max.) | Package |
|-------------|--------------------|-----------------------|---------|
| SARS01 | 1.2 A | 0.92 V | Axial |
| SARS05 | 1.0 A | 1.05 V | SJP |

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Absolute Maximum Ratings

| Unless otherwise specified, $T_A = 25$ Parameter | Symbol | Conditions | Rating | Unit | Remarks |
|---|--------------------|--|------------|------------------|---------|
| Nonrepetitive Peak Reverse Voltage | V _{RSM} | | 800 | V | |
| Repetitive Peak Reverse Voltage | V _{RM} | | 800 | V | |
| Average Forward Current ⁽¹⁾ | т | | 1.2 | | SARS01 |
| Average Forward Current | I _{F(AV)} | | 1.0 | A | SARS05 |
| | | Half cycle sine wave, | 110 | | SARS01 |
| Surge Forward Current | I _{FSM} | positive side, 10 ms, 1 shot | 30 | A | SARS05 |
| I ² t Limiting Value | I ² t | 1 | 60.5 | A ² s | SARS01 |
| I ² t Limiting Value | | $1 \text{ ms} \le t \le 10 \text{ ms}$ | 4.5 | A-S | SARS05 |
| Junction Temperature | TJ | | -40 to 150 | °C | |
| Storage Temperature | T _{STG} | | -40 to 150 | °C | |

Unless otherwise specified, $T_A = 25$ °C.

Electrical Characteristics

| Unless otherwise specified, $T_A = 25$ °C. | | | | | | | |
|---|----------------------|--|------|------|------|------|---------|
| Parameter | Symbol | Conditions | Min. | Тур. | Max. | Unit | Remarks |
| Formuard Voltage Drop | V _F | $I_F = 1.2 \text{ A}$ | | | 0.92 | v | SARS01 |
| Forward Voltage Drop | V F | $I_F = 1.5 A$ | | 0.91 | 1.05 | v | SARS05 |
| Powerse Leekage Current | I _R | V V | | | 10 | | SARS01 |
| Reverse Leakage Current | IR | $V_R = V_{RM}$ | | | 5 | μA | SARS05 |
| Reverse Leakage Current under High Temperature | $H \cdot I_R$ | $V_{R} = V_{RM},$ $T_{J} = 100 \ ^{\circ}C$ | | | 50 | μA | |
| Davana Davana Tima | | $I_F = I_{RP} = 10 \text{ mA},$ $T_J = 25 \text{ °C},$ 90% recovery point | 2 | | 18 | | SARS01 |
| Reverse Recovery Time | t _{rr} | $I_{F} = I_{RP} = 100 \text{ mA},$ $T_{J} = 25 \text{ °C},$ 90% recovery point | 2 | | 19 | μs | SARS05 |
| Thermal Resistance ⁽²⁾ | D | | | | 20 | °C/W | SARS01 |
| Thermal Resistance | R _{th(J-L)} | | | | 20 | C/ W | SARS05 |

Mechanical Characteristics

| Parameter | Conditions | Min. | Тур. | Max. | Unit | Remarks |
|----------------|------------|------|-------|------|------|---------|
| Package Weight | | | 0.2 | _ | g | SARS01 |
| | | | 0.072 | _ | g | SARS05 |



Figure 1. Lead Temperature Measurement Conditions

⁽¹⁾ See the derating curves of each product.

⁽²⁾ $R_{th(J-L)}$ is thermal resistance between junction and lead. Lead temperature (T_L) is measured near the root of pin (see Figure 1).

SARS01 Derating Curves



Figure 2. SARS01 $I_{F(AV)}$ vs. T_L (T_J = 150 °C, V_R = 0 V)

SARS01 Characteristic Curves



Figure 3. SARS01 $I_{F(AV)}$ vs. T_L ($T_J = 150$ °C, $V_R = 800$ V)

1.2 Maximum Forward Power Dissipation, P_{R(MAX)} (W) t/T = 1/6 1.0 t/T = 1/3, sine wave 0.8 t/T = 1/20.6 . DC 0.4 0.2 0.0 0.0 0.2 0.4 0.6 0.8 1.0 1.2 Average Forward Current, $I_{F(AV)}(A)$

Figure 4. SARS01 $P_{F(MAX)}$ vs. $I_{F(AV)}$ (T_J = 150 °C)



Figure 5. SARS01 $P_{R(MAX)}$ vs. V_R ($T_J = 150 \ ^{\circ}C$)





Figure 7. SARS01 Typical Characteristics: I_R vs. V_R



Figure 8. SARS01 Typical Transient Thermal Resistance Characteristics

SARS05 Derating Curves



SARS05 Characteristic Curves



Figure 11. SARS05 $P_{F(MAX)}$ vs. $I_{F(AV)}$ (T_J = 150 °C)



Forward Voltage Drop, $V_F(V)$

Figure 13. SARS05 Typical Characteristics: I_F vs. V_F



Figure 12. SARS05 $P_{R(MAX)}$ vs. V_R ($T_J = 150 \text{ °C}$)



Figure 14. SARS05 Typical Characteristics: I_R vs. V_R



Figure 15. SARS05 Typical Transient Thermal Resistance Characteristics

SARS01 Physical Dimensions and Marking Diagram

• SARS01 Physical Dimensions

Axial ($\varphi 2.7 \times 5.0L / \varphi 0.6$)



NOTES:

- Dimensions in millimeters
- Bare leads: Pb-free (RoHS compliant)
- The allowance position of Body against the center of whole lead wire is 0.5 mm (max.).
- The centric allowance of lead wire against center of physical body is 0.2 mm (max.).
- The burr may exit up to 2 mm from the body of lead.
- When soldering the products, it is required to minimize the working time, within the following limits: Flow: 260 °C, 10 s, 1 time

Soldering Iron: 350 °C, 3.5 s, 1 time (Soldering should be at a distance of at least 1.5 mm from the body of the product.)

• SARS01 Marking Diagram



Y is the last digit of the year of manufacture (0 to 9)

M is the month of the year (1 to 9, O, N, or D)

D is a period of days:

"•" is the first 10 days of the month (1st to 10th)

"••" is the second 10 days of the month (11th to 20th)

"••••" is the last 10–11 days of the month (21st to 31st)

SARS05 Physical Dimensions and Marking Diagram

• SARS05 Physical Dimensions





NOTES:

- Dimensions in millimeters
- Bare lead frame: Pb-free (RoHS compliant)
- Moisture Sensitivity Level 1 (MSL 1)
- When soldering the products, it is required to minimize the working time within the following limits: Flow: 260 $^{\circ}C$ / 10 s, 1 time

Reflow: Preheat: 150 °C to 200 °C / 60 s to 120 s Solder heating: 255 °C / 30 s, 3 times (260 °C peak) Soldering iron: 350 °C / 3.5 s, 1 time

• SARS05 Land Pattern Example



NOTE:

Dimensions in millimeters

• SARS05Marking Diagram



Operational Comparison of Clamp Snubber Circuits

Figure 16 shows a general clamp snubber circuit. In the circuit, the surge voltage at tuning off a power MOSFET is charged to C_S through the surge absorb loop, and is consumed by R_{S1} through the energy discharge loop. All the consumed energy becomes loss in R_{S1} . In addition, the ringing of surge voltage results in poor cross regulation of multi-outputs.



Figure 16. General Clamp Snubber Circuit



Figure 17. Waveforms of General Clamp Snubber Circuit



Figure 18. Enlarged View of Figure 17

Figure 19 shows the clamp snubber circuit using the SARS01/05. The surge voltage at tuning off a power MOSFET is charged to C_S through the surge absorb loop. Since the reverse recovery time, trr, of the SARS01/05 is a relatively long period, the energy charged to C_S is discharged to the reverse direction of the surge absorb loop until C_S voltage is equal to the flyback voltage. Some discharged energy is transferred to secondary side. Thus, the power supply efficiency improves.

In addition, the power supply using the SARS01/05 reduces the ringing voltage. Thus, the cross regulation of multi-outputs can be improved.



Figure 19. Clamp Snubber Circuit using SARS01/05



Figure 20. Waveforms of Clamp Snubber Circuit using SARS01



Figure 21. Enlarged View of Figure 20

Power Dissipation and Junction Temperature Calculation

Figure 22 shows a typical application using the SARS01/05. Figure 23 shows the operating waveforms of the SARS01/05. The power dissipation of the SARS01/05 is calculated as follows:

- 1) The waveforms of the SARS01/05 voltage, V_{SARS} , and the SARS01/05 current, I_{SARS} , are measured in actual application operation. $V_{SARS} \times I_{SARS}$ is calculated by the math function of oscilloscope.
- 2) The each average energy $(P_1, P_2 \cdots P_k)$ is measured at period of each polarity of $V_{SARS} \times I_{SARS}$ $(t_1, t_2, \cdots t_k)$ as shown in Figure 22 by the automatic measurement function of the oscilloscope.
- The power dissipation of the SARS01/05, P_{SARS}, is calucultated by Equation (1):

$$P_{SARS} = \frac{1}{T} (|P_1 \times t_1| + |P_2 \times t_2| + \dots |P_k \times t_k|)$$
(1)

where:

 P_{SARS} is power dissipation of the SARS01/05, T is switching cycle of power MOSFET (s), and P_k is average energy of period t_k (W).

A differential probe is recommended to use for the measurement of V_{SARS} . Please conform to the oscilloscope manual about power dissipation measurement including the delay compensation of probe. In addition, by using the temperature of the SARS01/05 in actual application operation, the estimated junction temperature of the SARS01/05 is calculated by Equation (2). It should be enough lower than T_J of the absolute maximum rating.

$$T_{J(SARS)} = T_{L} + \theta_{J-L} \times P_{SARS} (^{\circ}C)$$
(2)

where:

 $T_{J(SARS)}$ is junction temperature of the SARS01/05, T_L is lead temperature of the SARS01/05, and θ_{J-L} is thermal resistance between junction to lead.



Figure 22. Typical Application



Figure 23. SARS01/05 Current

Parameter Setting of Snubber Circuit using SARS01/05

The temperature of the SARS01/05 and peripheral components should be measured in actual application operation.

The reference values of snubber circuit using the SARS01/05 are as follows:

• Cs

680 pF to 0.01 $\mu F.$

The voltage rating is selected according to the voltage subtraced the input voltage from the peak of V_{DS} .

• **R**_{S1}

 R_{S1} is the bias resistance to turn off the SARS01/05, and is 100 k\Omega to 1 M\Omega.

Since a high voltage is applied to R_{S1} that has high resistance, the following should be considered according to the requirement of the application:

- Select a resistor designed for electromigration, or
- Connect more resistors in series so that the applied voltages of individual resistors can be reduced.

The power rating of resistor should be selected from the measurement of the effective current of R_{S1} based on actual operation in the application.

• **R**_{S2}

 R_{S2} is the limited resistance in the energy discharging. The value of 22 Ω to 220 Ω is connected to the SARS01/05 in series.

The power rating of resistor should be selected from the measurement of the effective current of R_{S2} based on actual operation in the application.

Reference Design of Power Supply

This section provides the information on a reference design, including power supply specifications, a circuit diagram, the bill of materials, and transformer specifications.

• Power Supply Specifications

| Item | Specification |
|---------------|---------------------------|
| Input Voltage | 85 VAC to 265 VAC |
| Output Power | 34.8 W (40.4 W peak) |
| Output 1 | 8 V / 0.5 A |
| Output 2 | 14 V / 2.2 A (2.6 A peak) |

• Circuit Schematic



• Bill of Materials

| - 5111 01 | Matchais | | | | |
|--------------------|-----------------------------|----------------------|--------------------|------------------------------------|----------------------|
| Symbol | Ratings ⁽¹⁾ | Recommended Part No. | Symbol | Ratings ⁽¹⁾ | Recommended Part No. |
| C1 ⁽²⁾ | Film, 0.1 µF, 275 V | | D52 | Schottky, 100 V, 20 A | FMEN-220A |
| C2 ⁽²⁾ | Electrolytic, 150 µF, 400 V | | F1 | Fuse, 250 V AC, 3 A | |
| C3 | Ceramic, 1000 pF, 1 kV | | L1 ⁽²⁾ | CM inductor, 3.3 mH | |
| C4 | Ceramic, 0.01 µF | | PC1 | Optocoupler, PC123 or equiv. | |
| C5 | Electrolytic, 22 µF, 50 V | | R1 ⁽³⁾ | Metal oxide, 330 kΩ, 1 W | |
| C6 ⁽²⁾ | Ceramic, 15 pF / 2 kV | | R2 | 47 Ω, 1 W | |
| C7 ⁽²⁾ | Ceramic, 2200 pF, 250 V | | R3 | 10 Ω | |
| C51 ⁽²⁾ | Electrolytic, 680 µF, 25 V | | R4 ⁽²⁾ | 0.47 Ω, 1/2 W | |
| C52 | Electrolytic, 680 µF, 25 V | | R51 | 1 kΩ | |
| C53 | Electrolytic, 470 µF, 16 V | | R52 | 1.5 kΩ | |
| C54 ⁽²⁾ | Ceramic, 0.1 µF, 50 V | | R53 ⁽²⁾ | 100 kΩ | |
| D1 | 600 V, 1 A | EM01A | R54 ⁽²⁾ | 6.8 kΩ | |
| D2 | 600 V, 1 A | EM01A | R55 | \pm 1%, 39 k Ω | |
| D3 | 600 V, 1 A | EM01A | R56 | \pm 1%, 10 k Ω | |
| D4 | 600 V, 1 A | EM01A | T1 | See the Transformer | |
| D5 | | GAD 605 | 111 | Specification | 0770244520 |
| D5 | 800 V, 1.0 A | SARS05 | U1 | IC | STR3A453D |
| D6 | Fast recovery, 200 V, 1.5A | SJPX-F2 | U51 | Shunt regulator, $V_{REF} = 2.5 V$ | (TL431 or equiv.) |
| D51 | Schottky, 60 V, 1.5 A | SJPB-H6 | | | |
| (1) | | | | | |

⁽¹⁾ Unless otherwise specified, the voltage rating of capacitor is 50 V or less and the power rating of resistor is 1/8 W or less.

⁽²⁾ Refers to a part that requires adjustment based on operation performance in an actual application.

(3) High voltage is applied to this resistor that has high resistance. To meet your application requirements, it is required to select resistors designed for electromigration, or to connect more resistors in series so that the applied voltages of individual resistors can be reduced.

• Transformer Specifications

| Item | Specification |
|------------------------|--|
| Primary Inductance, LP | 518 µH |
| Core Size | EER-28 |
| AL Value | 245 nH/N ² (with a center gap of about 0.56 mm) |
| Winding Specification | See Table 1 |
| Winding Structure | See Figure 24 |

Table 1. Winding Specification

| Winding | Symbol | Number of Turns (turns) | Wire Diameter (mm) | Structure |
|-------------------|--------|----------------------------|-----------------------|--------------------------------|
| Primary Winding | P1 | 18 | $\phi 0.23 \times 2$ | Single-layer, solenoid winding |
| Primary Winding | P2 | 28 | φ 0.30 | Single-layer, solenoid winding |
| Auxiliary Winding | D | 12 | $\phi 0.30 \times 2$ | Solenoid winding |
| Output 1 Winding | S1-1 | 6 | $\phi 0.4 \times 2$ | Solenoid winding |
| Output 1 Winding | S1-2 | 6 | $\phi 0.4 \times 2$ | Solenoid winding |
| Output 2 Winding | S2-1 | 4 | $\phi \ 0.4 \times 2$ | Solenoid winding |
| Output 2 Winding | S2-2 | 4 | $\phi \ 0.4 \times 2$ | Solenoid winding |



Figure 24. Winding Structure

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